

## ERRATA – Vol 1

**1. p. 3-6, 2nd full paragraph, 4th line:**

RCRA Subpart **Subtitle C** . . . .

**2. p. 3-21, 4th line, middle of line:**

. . . RCRA Subpart **Subtitle D** landfills.

**3. p. 3-23, last paragraph before bullet items, 3rd line, middle of line:**

. . . RCRA Subpart **Subtitle D** disposal facility . . . .

**p. 3-23, footnote 30:**

Although EPA regulations would allow the stabilized dust to be disposed of in a RCRA Subpart **Subtitle D** (non-hazardous) landfill, these two facilities conform to the requirements of RCRA Subpart **Subtitle C** for hazardous waste disposal.

**4. p. 3-25, Section 3.2.4.2, 1st line below 5 bullet items:**

Presumably, the unsold balance of about ~~5.5~~ 7.9 Mt is either recycled to a sinter plant or landfilled after recovery of metal values.

**5. p. 3-39, Section 3.6.1.1, last definition following Equation 3.6:**

$t_s$  = interval from time scrap is cleared until scenario begins (d)

**6. p. 3-40, Section 3.6.1.2, Equation 3.7, change  $f_{ix}$  to  $F_{ix}$ :**

$$D_{ix} = C_{ij} F_{ix} t_{xy} \left( \frac{e^{-\lambda_i t_s} - e^{-\lambda_i (t_s + t_a)}}{\lambda_i t_a} \right) \quad 3.7$$

**7. p. 3-44, Notes to Table 3.10, c:**

19 Steel ship: (a) berthing, (b) mess and lounge, ⊕ (c) operations, (d) deck

8. p. 3-45, Equation 3.10, change  $t_{dy}$  to  $t_{ys}$

$$D_{ix} = C_{ig} F_{ix} S_{vx} t_{xd} t_{ys} U_x e^{-\lambda_i t_s} \quad 3.10$$

Add after last definition:

$$t_{ys} = \text{exposure duration (d/y)}$$

9. p. 3-61, after equation at top of page:

$$t_{dw} = \text{time in driver's seat hauling driving with one-way load (h/w)}$$

10. p. 3-74. Section 3.7.6, 1st paragraph, 5th line, middle of line:

... RCRA Subpart Subtitle C . . . .

2nd paragraph:

Hazardous waste landfills fall under RCRA Subpart Subtitle C. According to current practices, as discussed in Section 3.2.4.1, EAF dust placed in a Subpart Subtitle C landfill . . . .

11. p. 3-89, 2nd line of Equation 3.39: change  $K_a$  to  $K_{sa}$

$$\begin{aligned} dC_{wi}(\tau) &= C_{ip}(\tau) df \\ &= \frac{C_{ig} d_g f_i'(\tau) \rho_g}{\delta_w J K_{sa}} dx \\ &= \frac{C_{ig} d_g f_i'(\tau) \rho_g}{\delta_w p_e' R_{di}'} d\tau \end{aligned} \quad 3.39$$

12. p. 3-94, Section 3.8.1, 1st paragraph, 5th line:

general types of BWR reactor components—rebar, structural steel, and pipe hangers—are judged to be

Delete next to last sentence:

range of sizes. Each size has a different mass-to-surface ratio. Four types of PWR components—the three BWR types plus piping—are judged to be candidates for clearance. The

**13. p. 4-19, 1st line:**

The mean and the 5th, 50th, 90th, and 95th percentile radionuclide concentrations in the products of . . . .

**14. p. 4-20, Table 4.7, last two rows:**

Leachate–industrial– <del>cross</del> slag	Leachate from industrial landfill–slag	mod	IL			●
Leachate–municipal– <del>cross</del> slag	Leachate from municipal landfill–slag	mod	ML			●

**15. p. 4-43, 2nd reference on page:**

Gößling, S. 2001. “Entropy Balance of Industrial Copper Production: A Measure for Resource Use: First Results for Flash Smelting, Converting and Refining.”  
<http://www.desy.de/~stefang/beschreibung.html> (September 13, 2000 2002).